## HIGH REYNOLDS NUMBER LARGE EDDY SIMULATION: WHERE REAL AND VIRTUAL TURBULENCE MEET?

#### Peter P. Sullivan

**National Center for Atmospheric Research** 

NCAR is sponsored by the National Science Foundation Support from Office of Naval Research

## HIGH RESOLUTION GLOBAL SIMULATION Courtesy J. Hurrell and CGD/NCAR



AN ABUNDANCE OF TIME AND SPACE SCALES!

## **BOUNDARY-LAYER PROCESSES**



Stably stratified turbulent flow just above a walnut orchard during the Canopy Horizontal Array Turbulence Study (CHATS)



## Provided by Shane Mayor & Ned Patton

LidarPPI Display Version 1.7.1

PPI Mode, Transect 3, El: 0.2

## **SCALES OF TURBULENCE RELATIVE TO NWP SCALES**



**Courtesy Anton Beljaars (ECMWF)** 

## LOW LEVEL FLIGHT IN HURRICANE ISABEL Courtesy M. Black

$$v_{max}^2 = \frac{T_s - T_o}{T_o} \frac{C_k}{C_D} (k_s^* - k)$$

Maximum azimuthal wind speed (Emanuel, 2004)

9

z (cm)

9

•

10

z (cm)

#### C<sub>D</sub> Donelan etal, 2004



x (cm)

30

40

20

## **SPIRALS ON THE SEA**



Photograph of a cyclonic spiral-eddy street off the coast of the Egyptian/Libyan border. Eddy radii are  $\approx$  5 km, and scum convergence lines are  $\sim$  100s m wide. The street configuration suggests a recent vortex roll-up from an unstable submesoscale front or wake. (Scully-Power, 1986), courtesy J. McWilliams.

## **OCEAN WEATHER SYSTEMS**



Simulated vertical vorticity normalized by f illustrating the interaction between fronts, instabilities and vortices in the ocean. Courtesy J. McWilliams (UCLA)

## SUMMARY OF SUBMESOSCALE TURBULENCE Courtesy Jim McWilliams (UCLA)

- Surface-intensified frontogenesis induced by mesoscale straining
- Frontal instabilites of several types
- Kinetic energy forward cascade towards turbulence dissipation



AN EXAMPLE OF AN MPAS MESH BASED ON SPHERICAL CENTROIDAL VORONOI TESSELLATIONS http://public.lanl.gov/ringler/Voronoi.html



A need for scale aware parameterizations?

# What are the appropriate (LES) equations for Terra-Incognita?



## **TOO MANY SCALES!**



## **GOVERNING EQUATIONS**

Given incompressible Navier Stokes equations:

$$\frac{\partial u_i}{\partial t} + \frac{\partial u_i u_j}{\partial x_j} = -\frac{1}{\rho} \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j^2}$$

## COMMENTS ON THE FILTERED EQUATIONS AND THE SUBGRID SCALE STRESS TENSOR

$$\frac{\partial \overline{u}_{i}}{\partial t} + \frac{\partial \overline{u}_{i}\overline{u}_{j}}{\partial x_{j}} = -\frac{1}{\rho}\frac{\partial \overline{p}}{\partial x_{i}} - \frac{\partial}{\partial x_{j}}\left(\tau_{ij} - \nu\frac{\partial \overline{u}_{i}}{\partial x_{j}}\right) 
\tau_{ij} = \overline{u_{i}u_{j}} - \overline{u}_{i}\overline{u}_{j}$$

- The filtered equations are generally applicable in the LES and mesoscale limits and also in Terra-Incognita [Lilly(1967)]
- The filtered equations contain two parameters, molecular viscous Reynolds number and the SGS stress tensor  $T_{ij}$
- $T_{ij}$  is unknown! It needs to be expressed in terms of known resolved fields  $\overline{u}_i$
- $T_{ij}$  controls how the flow transitions from mesoscale limit  $\iff$  LES limit

## **RESOLVED FLOW IN MESOSCALE LIMIT**

Simple eddy viscosity closure (model for deviatoric stress)

$$\tau_{ij} \sim K\left(\frac{\partial \overline{u}_i}{\partial x_j} + \frac{\partial \overline{u}_j}{\partial x_i}\right), \quad K = e^{1/2}l$$

In mesoscale limit:  $L_{turb} < \triangle_f$ 



## **RESOLVED FLOW IN LES LIMIT**

Simple eddy viscosity closure (model for deviatoric stress)

$$\tau_{ij} \sim K\left(\frac{\partial \overline{u}_i}{\partial x_j} + \frac{\partial \overline{u}_j}{\partial x_i}\right), \quad K = e^{1/2}l$$



In LES limit:  $\triangle_f < L_{turb}$ 



Suggested behavior of the length scale  $\ell$  of the unresolved turbulence as function of  $\Delta_f$  for a K-model

## HOW DOES ENERGY FLOW BETWEEN RESOLVED AND SGS FIELDS?



## HOW DOES ENERGY FLOW BETWEEN RESOLVED AND SGS FIELDS?

• Need to build energy transport equations:

Resolved energy 
$$\overline{u}_i \frac{\partial \overline{u}_i}{\partial t} = \dots - \overline{u}_i \frac{\partial \tau_{ij}}{\partial x_j}$$
  

$$= \dots \tau_{ij} \frac{1}{2} \left( \frac{\partial \overline{u}_i}{\partial x_j} + \frac{\partial \overline{u}_j}{\partial x_i} \right)$$

$$= \dots \tau_{ij} S_{ij}$$
Energy transfer term  
SGS energy  $\overline{u_i \frac{\partial u_i}{\partial t}} - \overline{u}_i \frac{\partial \overline{u}_i}{\partial t} = \dots - \tau_{ij} S_{ij} - \epsilon$ 
Molecular dissipation

## DO HIGH-Re ROUGH-WALL LES STATISTICS CONVERGE WITH MESH REFINEMENT?





**8** am

Local time

Noon

**Courtesy Shane Mayor** 

 $Re_{\mathcal{L}} = \mathcal{UL}/\nu = 10^8$ 

#### LES EQUATIONS FOR DRY ATMOSPHERIC PBL



Subgrid-scale momentum and scalar fluxes

$$egin{array}{rcl} {f T}&=&\overline{u_i\,u_j}\,-\,\overline{u_i}\,\overline{u_j}\ {f B}&=&\overline{u_i\,b}\,-\,\overline{u_i}\,\overline{b} \end{array}$$

Incompressible Boussinesq flow

$$\nabla \cdot \overline{\mathbf{u}} = 0 \implies \nabla^2 \pi = s$$

## DO LES STATISTICS CONVERGE WITH MESH REFINEMENT?



## **FREE CONVECTION 512<sup>3</sup> W-FIELD**



## LES OF CONVECTIVE PBL, 4096 CPUS, 1024<sup>3</sup> GRIDPOINTS



## DUST DEVILS in TALAMAKAN DESERT OF CHINA Courtesy of Don Lenschow NCAR



#### **DO LES STATISTICS CONVERGE WITH MESH REFINEMENT?**



#### **PBL HEIGHT** $z_i$ FOR VARYING MESHES



Entrainment rate  $w_e = dz_i/dt$  decreases with increasing mesh resolution

#### **IMPACT OF GRID RESOLUTION ON SKEWNESS**



Can we use targeted observations to provide insight as to the nature of SGS motions in high Re PBLs?

## HIGH REYNOLDS NUMBER OBSERVATIONS AND LES

#### • SINGLE-POINT MEASUREMENTS

- Cannot be used directly to improve LES

#### MULTI-POINT MEASUREMENTS



- Span a range of filter widths,  $e.g., \mathcal{O}(m)$  to  $\mathcal{O}(100m)$
- Ideally 3-D, time varying "volume" of turbulence and scalars in canonical flows with shear, stratification, near boundaries, ...
- Horizontal Array Turbulence Study field campaigns, HATS (2000), OHATS (2004), CHATS (2007), AHATS (2008)

## HATS CONFIGURATIONS

 $\sim 36 \ cases$ -1.2 < z/L < 1.6 $0.15 < \Lambda_w/\Delta_f < 15$ 









#### RATIONALE FOR EXPERIMENTAL DESIGN

$$U_i = \overline{U_i} + u_i \equiv \int U(x'_j) G(x_i, x'_j) dx'_j + u_i$$

• Allows construction of SFS fluxes:

$$\mathcal{T}_{ij} = \overline{U_i U_j} - \overline{U_i} \ \overline{U_j}$$

- Allows measurement of resolved gradients  $\partial \overline{U_i}/\partial x$ ,  $\partial \overline{U_i}/\partial y$  and  $\partial \overline{U_i}/\partial z$
- Allows expansion of SFS fluxes  $T_{ij}$  into Leonard, Cross, and Reynolds terms which requires *double* spatial filtering, *e.g.*,  $\overline{\overline{U_i}u_j}$

## **AN EXAMPLE OF LATERAL (Y) FILTERING**







## **AN EXAMPLE OF LATERAL (Y) FILTERING**





## **AN EXAMPLE OF LATERAL (Y) FILTERING**





## SPECTRAL PEAK AND FILTER CUTOFF WAVENUMBERS





#### **SFS VELOCITY VARIANCES**



#### **RATE EQUATIONS FOR SUBGRID DEVIATORIC STRESS**

• What are the parent equations for the Smagorinsky model?

## **RATE EQUATIONS FOR SUBGRID DEVIATORIC STRESS**

#### • What are the parent equations for the Smagorinsky model?

Lilly (1967), Deardorff (1973), Wyngaard (2004), Hatlee & Wyngaard (2007)
 Germano (1992)

$$\frac{D\tau_{ij}}{Dt} = \frac{2}{3}e\left(\frac{\partial\overline{u}_i}{\partial x_j} + \frac{\partial\overline{u}_j}{\partial x_i}\right) \qquad \text{Isotropic production} \\
- \left[\tau_{ik}\frac{\partial\overline{u}_j}{\partial x_k} + \tau_{jk}\frac{\partial\overline{u}_i}{\partial x_k} - \frac{1}{3}\delta_{ij}\tau_{kl}\left(\frac{\partial\overline{u}_k}{\partial x_l} + \frac{\partial\overline{u}_l}{\partial x_k}\right)\right] \\
- \frac{1}{\rho}\left[p\left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right) - \overline{p}\left(\frac{\partial\overline{u}_i}{\partial x_j} + \frac{\partial\overline{u}_j}{\partial x_i}\right)\right] \\
+ \text{ transport + buoyancy production}$$

Pressure destruction

Anisotropic deviatoric production

#### **RATE EQUATIONS FOR SUBGRID DEVIATORIC STRESS**

#### • What are the parent equations for the Smagorinsky model?

- Lilly (1967), Deardorff (1973), Wyngaard (2004), Hatlee & Wyngaard (2007)

$$\frac{D\tau_{ij}}{Dt}^{0} = \frac{2}{3}e\left(\frac{\partial\overline{u}_{i}}{\partial x_{j}} + \frac{\partial\overline{u}_{j}}{\partial x_{i}}\right) \\
- \left[\tau_{ik}\frac{\partial\overline{u}_{j}}{\partial x_{k}} + \frac{\partial\overline{u}_{i}}{\tau_{jk}}\frac{1}{\partial x_{k}} - \frac{1}{3}\delta_{ij}\tau_{kl}\left(\frac{\partial\overline{u}_{k}}{\partial x_{l}} + \frac{\partial\overline{u}_{l}}{\partial x_{k}}\right)\right]^{0} \\
- \frac{1}{\rho}\left[p\left(\frac{\partial u_{i}}{\partial x_{j}} + \frac{\partial u_{j}}{\partial x_{i}}\right) - \overline{p}\left(\frac{\partial\overline{u}_{i}}{\partial x_{j}} + \frac{\partial\overline{u}_{j}}{\partial x_{i}}\right)\right] \quad \text{Rotta model} \\
+ \text{transport} + \text{buoyancy production}$$

Time scale

 $T = c \frac{\Delta_f}{\sqrt{e}}$ 

$$rac{ au_{ij}}{T} \;=\; rac{2}{3} e \left( rac{\partial \overline{u}_i}{\partial x_j} \;+\; rac{\partial \overline{u}_j}{\partial x_i} 
ight)$$

## **PRODUCTION OF SUBFILTER SCALE FLUX** $\tau_{11}$





**PRODUCTION OF SUBFILTER SCALE FLUX**  $\tau_{13}$ 



Decomposition of SFS Production into Forwardscatter and Backscatter

$$P = -\mathcal{T}_{ij}S_{ij}$$
  $P_f = (P + |P|)/2$   $P_b = (P - |P|)/2$ 

## Decomposition of SFS Production into Forwardscatter and Backscatter



 $P = -\mathcal{T}_{ij}S_{ij}$   $P_f = (P + |P|)/2$   $P_b = (P - |P|)/2$ 

## SUMMARY

- Atmospheric and oceanic boundary-layer dynamics are unique compared to flat-wall boundary layers because of surface waves
  - Winds, currents, drag, variances, dissipation, entrainment, ...
- Carefully crafted high Re LES neatly exposes the interactions between winds-waves, waves-currents
- LES solutions for means and second-order moments converge with mesh refinement provided  $z_i/C_s \triangle_f > 300$  (for daytime convective BL)
  - Solutions exhibit approximate Reynolds-number similarity
  - Entrainment rate decreases with increasing mesh resolution
  - Vertical velocity skewness is an indicator of mesh sensitivity
- Measurements of subgrid-scale variables show SGS (eddy viscosity) parameterizations used in LES are inadequate when the ratio  $\Lambda/\triangle_f \sim \mathcal{O}(1)$  or less
  - Anisotropic production of scalar and momentum flux in surface layers is important
- Yes! LES is exceedingly useful, but can be improved

## AN LES PROPOSAL TO STUDY TERRA-INCOGNITA DYNAMICS

- Run big with conventional LES! Processor counts  $\sim \mathcal{O}(10^4)$  or more
- Design LES with a minimum (tolerable) resolution say  $L_{turb}/\triangle_f \sim 20$  then choose  $N_{points}$  large to capture key large-scale processes
- To be interesting  $N_{points}$  needs to be large enough to capture  $L_{turb}/\triangle_f = 1$
- A-prior filtering of LES databases at Terra-Incognita resolutions, say  $L_{turb}/\delta_f = [10, 1, 0.5, 0.1]$  where  $\delta_f > \triangle_f$
- Others are doing this in the atmosphere and ocean, *e.g.*, [Moeng and Arakawa(2012)], Baylor Fox-Kemper *et al.*(2012) on Yellowstone
- Dissect the Horizontal Array Turbulence Studies carried out in the atmospheric surface layer